



Studijski program:

GRAĐEVINARSTVO

Modul:

PŽA, HVE, MTI

Godina/Semestar:

III godina / V semestar

Naziv predmeta (šifra):

Betonske konstrukcije 1

(B2S3BK, B2H3BK, B2M3BK, B1S3BK)

Nastavnik:

Jelena Dragaš

Naslov predavanja:

Dimenzionisanje stubova

Datum :

24.11.2022.

Beograd, 2021.

Zadatak 19 – KOMBINOVANJE OPTEREĆENJA

Odrediti potrebnu površinu armature za stub poznatih dimenzija, pravougaonog poprečnog preseka, opterećen zadatim uticajima. Podaci za proračun:

$$M_G = 100 \text{ kNm}$$

$$N_G = 500 \text{ kN}$$

$$M_w = \pm 200 \text{ kNm}$$

$$b = 25 \text{ cm}$$

$$h = 65 \text{ cm}$$

C25/30

B500 B



a1. zategnuta spoljašnja ivica stuba – Nmax

$$M_{Ed} = 1.35 \times 100 + 1.5 \times 200 = 435 \text{ kNm}$$

$$N_{Ed} = 1.35 \times 500 = 675 \text{ kN}$$

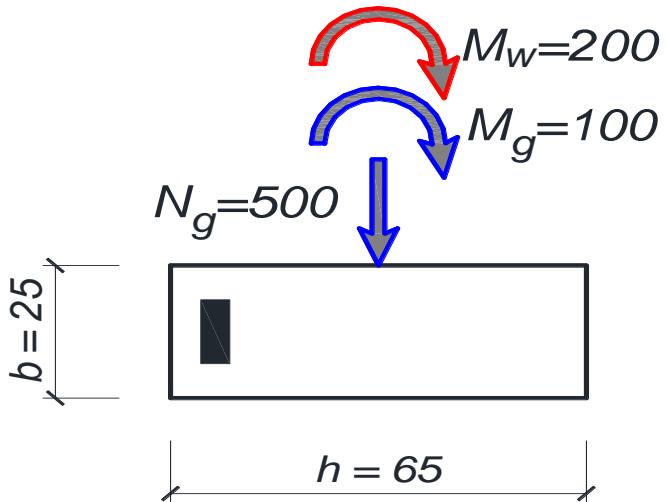
pretp. $d_1 = 7 \text{ cm}$

$$d = 65 - 7 = 58 \text{ cm}$$

$$\text{C25/30} \Rightarrow f_{cd} = 14.2 \text{ MPa}$$

$$M_{Eds} = 435 + 675 \times \left(\frac{0.65}{2} - 0.07 \right) = 607.1 \text{ kNm}$$

$$k = \frac{58}{\sqrt{\frac{607.1 \times 10^2}{25 \times 1.42}}} = 1.402 \Rightarrow \varepsilon_{s1} < 2.5\%$$



Kako je $\varepsilon_{s1} < 2.5\%$, presek se OBOSTRANO ARMIRA.



usvojeno $\varepsilon_{s1,lim} = 2.5\%$ $\Rightarrow k_{lim} = 1.672$, $\omega_{Rd,lim} = 47.222\%$

$$M_{Rd,lim} = \left(\frac{58}{1.672} \right)^2 \times 25 \times 1.42 \times 10^{-2} = 427.2 \text{ kNm}$$

$$\Delta M = 607.1 - 427.2 = 179.9 \text{ kNm}$$

$$pretp.d_2 = 5 \text{ cm} \Rightarrow A_{s2} = \frac{179.9 \times 10^2}{(58 - 5) \times 43.5} = 7.8 \text{ cm}^2$$

$$\varepsilon_{s2} = \frac{\xi_{lim} - \frac{d_2}{d}}{\xi_{lim}} \varepsilon_{cu2} = \frac{0.584 - \frac{5}{58}}{0.584} \cdot 3.5 = 2.98 > 2.175 = \frac{435}{200} \left(= \frac{f_{yd}}{E_s} \right) \quad \textcolor{red}{A_{s1} > A_{s2}}$$

$$A_{s1} = 47.222 \times \frac{25 \times 58}{100} \times \frac{1.42}{43.5} - \frac{675}{43.5} + 7.8 = 14.63 \text{ cm}^2$$



a1. zategnuta spoljašnja ivica stuba – Nmin

$$M_{Ed} = 1.0 \times 100 + 1.5 \times 200 = 400 \text{ kNm}$$

$$N_{Ed} = 1.0 \times 500 = 500 \text{ kN}$$

pretp. $d_1 = 7 \text{ cm}$

$$d = 65 - 7 = 58 \text{ cm}$$

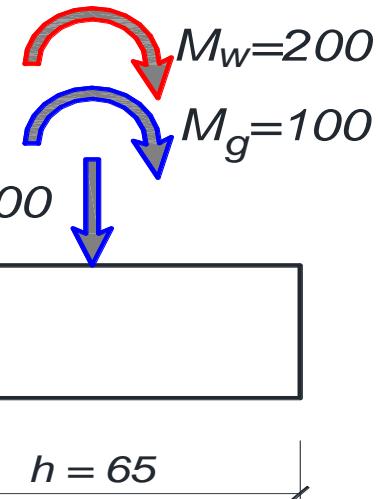
**“povoljno”
dejstvo stalnog
opterećenja**

$$\text{C25/30} \Rightarrow f_{cd} = 14.2 \text{ MPa}$$

$$M_{Eds} = 400 + 500 \times \left(\frac{0.65}{2} - 0.07 \right) = 527.5 \text{ kNm}$$

$$k = \frac{58}{\sqrt{\frac{527.5 \times 10^2}{25 \times 1.42}}} = 1.504 \Rightarrow \varepsilon_{s1} < 2.5\%$$

Kako je $\varepsilon_{s1} < 2.5\%$, presek se OBOSTRANO ARMIRA.



usvojeno $\varepsilon_{s1,lim} = 2.5\%$ $\Rightarrow k_{lim} = 1.672$, $\omega_{Rd,lim} = 47.222\%$

$$M_{Rd,lim} = \left(\frac{58}{1.672} \right)^2 \times 25 \times 1.42 \times 10^{-2} = 427.2 \text{ kNm}$$

$$\Delta M = 527.5 - 427.2 = 100.3 \text{ kNm}$$

$$pretp.d_2 = 5 \text{ cm} \Rightarrow A_{s2} = \frac{100.3 \times 10^2}{(58 - 5) \times 43.5} = 4.35 \text{ cm}^2$$

$$\varepsilon_{s2} = \frac{\xi_{lim} - \frac{d_2}{d}}{\xi_{lim}} \varepsilon_{cu2} = \frac{0.584 - \frac{5}{58}}{0.584} \cdot 3.5 = 2.98 > 2.175 = \frac{435}{200} \left(= \frac{f_{yd}}{E_s} \right)$$

$$A_{s1} = 47.222 \times \frac{25 \times 58}{100} \times \frac{1.42}{43.5} - \frac{500}{43.5} + 4.35 = 15.21 \text{ cm}^2$$



a1. Mmax, Nmax

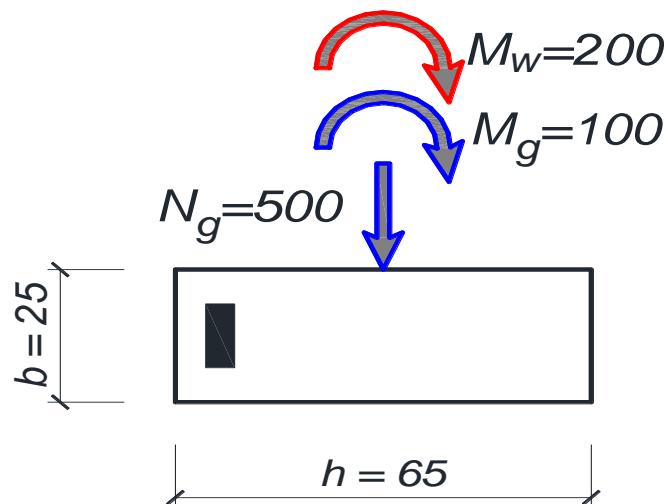
$$A_{s1} = 14.63 \text{ cm}^2$$

$$A_{s2} = 7.8 \text{ cm}^2$$

a2. Mmax, Nmin

$$A_{s1} = 15.21 \text{ cm}^2$$

$$A_{s2} = 4.35 \text{ cm}^2$$



b. zategnuta unutrašnja ivica stuba – Nmin

$$M_{Ed} = 1.0 \times (-100) + 1.5 \times 200 = 200 \text{ kNm}$$

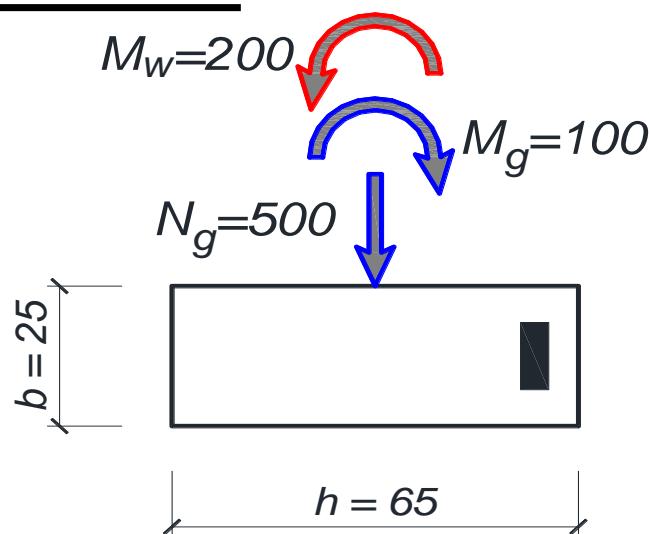
$$N_{Ed} = 1.0 \times 500 = 500 \text{ kN}$$

pretp. $d_1 = 5 \text{ cm}$

$$d = 65 - 5 = 60 \text{ cm}$$

$$\text{C25/30} \Rightarrow f_{cd} = 14.2 \text{ MPa}$$

“povoljno” dejstvo stalnog opterećenja



$$M_{Eds} = 200 + 500 \times \left(\frac{0.65}{2} - 0.05 \right) = 337.5 \text{ kNm}$$

$$k = \frac{60}{\sqrt{\frac{337.5 \times 10^2}{25 \times 1.42}}} = 1.946 \Rightarrow \frac{\varepsilon_c / \varepsilon_{s1}}{\omega_1} = \frac{3.5 / 5.435\%}{31.646\%}$$

$$A_{s1} = 31.646 \times \frac{25 \times 60}{100} \times \frac{1.42}{43.5} - \frac{500}{43.5} = 4.0 \text{ cm}^2$$



b. zategnuta unutrašnja ivica stuba – Nmax

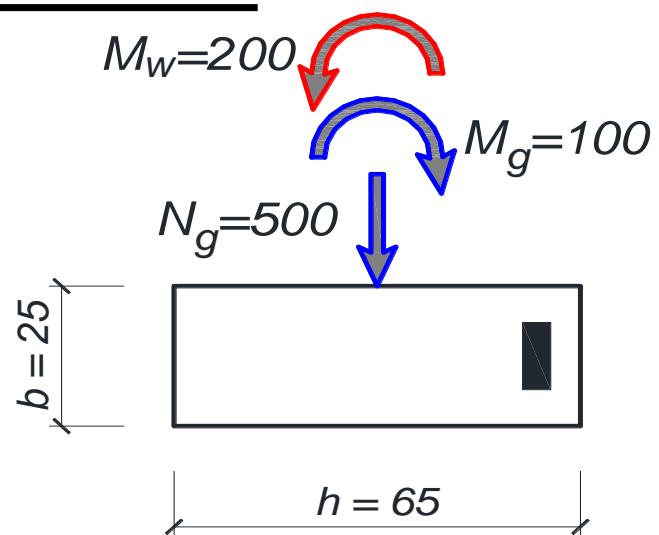
$$M_{Ed} = 1.35 \times (-100) + 1.5 \times 200 = 165 \text{ kNm}$$

$$N_{Ed} = 1.35 \times 500 = 675 \text{ kN}$$

pretp. $d_1 = 5 \text{ cm}$

$$d = 65 - 5 = 60 \text{ cm}$$

$$\text{C25/30} \Rightarrow f_{cd} = 14.2 \text{ MPa}$$



$$M_{Eds} = 165 + 675 \times \left(\frac{0.65}{2} - 0.05 \right) = 350.6 \text{ kNm}$$

$$k = \frac{60}{\sqrt{\frac{350.6 \times 10^2}{25 \times 1.42}}} = 1.909 \Rightarrow \begin{aligned} \varepsilon_c / \varepsilon_{s1} &= 3.5 / 5.0\% \\ \omega_1 &= 33.333\% \end{aligned}$$

$$A_{s1} = 33.333 \times \frac{25 \times 60}{100} \times \frac{1.42}{43.5} - \frac{675}{43.5} = 0.8 \text{ cm}^2$$



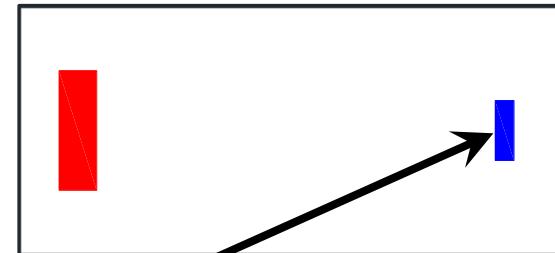
14.63
15.21

7.8
4.35



POTREBNO:

15.21 7.8



unutra : $A_{s,potr.} = \max.\left\{\frac{7.8}{4.0}\right\} = 7.8 \text{ cm}^2$

usvojeno: **3Ø20** (9.42 cm^2)

spolja : $A_{s,potr.} = 15.21 \text{ cm}^2$

$$A_{s1,min} = \begin{cases} 0.26 \cdot \frac{2.6}{500} \cdot 25 \cdot 60 = 2.0 \text{ cm}^2 \\ 0.0013 \cdot 25 \cdot 60 = 1.95 \text{ cm}^2 \end{cases}$$

usvojeno: **5Ø20** (15.7 cm^2)

$$A_{s1,min} = 2.0 \text{ cm}^2$$

Zadatak 20 – KOMBINOVANJE OPTEREĆENJA

*Dimenzionisati stub poznatih dimenzija, pravougaonog poprečnog preseka, opterećen zadatim uticajima. Opterećenja **q** i **w** su povremena i NE MORAJU delovati istovremeno.*

Podaci za proračun:

$$M_G = 100 \text{ kNm}$$

$$N_Q = 500 \text{ kN}$$

$$M_w = \pm 200 \text{ kNm}$$

$$b = 25 \text{ cm}$$

$$h = 65 \text{ cm}$$

C25/30

B500B



KOMBINACIJE OPTERECENJA

Promenljiva dejstva na stambene zgrade				
Promenljivo dejstvo	Korisno opterećenje	Sneg na krovu	Vetar	
Karakteristična vrednost, Q_k	$Q_{k,es}$	$Q_{k,n}$	$F_{k,w}$	
Vrednost za kombinaciju, za granično stanje nosivosti, $\Psi_0 \cdot Q_k$	$0.7 \cdot Q_{k,es}$	$0.5 \cdot Q_{k,n}$	$0.6 \cdot F_{k,w}$	

- Dominantno promenljivo dejstvo: KORISNO

$$1,35 \cdot G_k + 1,5 \cdot (Q_{k,es} + 0,5 \cdot Q_{k,n} + 0,6 \cdot F_{k,w}) = 1,35 \cdot G_k + 1,5 \cdot Q_{k,es} + 0,75 \cdot Q_{k,n} + 0,9 \cdot F_{k,w}$$

- Dominantno promenljivo dejstvo: SNEG

$$1,35 \cdot G_k + 1,5 \cdot (Q_{k,n} + 0,7 \cdot Q_{k,es} + 0,6 \cdot F_{k,w}) = 1,35 \cdot G_k + 1,5 \cdot Q_{k,n} + 1,05 \cdot Q_{k,es} + 0,9 \cdot F_{k,w}$$

KOMBINACIJE OPTERECENJA

Promenljiva dejstva na stambene zgrade			
Promenljivo dejstvo	Korisno opterećenje	Sneg na krovu	Vetar
Karakteristična vrednost, Q_k	$Q_{k,es}$	$Q_{k,n}$	$F_{k,w}$
Vrednost za kombinaciju, za granično stanje nosivosti, $\Psi_0 \cdot Q_k$	$0.7 \cdot Q_{k,es}$	$0.5 \cdot Q_{k,n}$	$0.6 \cdot F_{k,w}$

- Dominantno promenljivo dejstvo: VETAR

$$1,35 \cdot G_k + 1,5 \cdot (F_{k,w} + 0,5 \cdot Q_{k,n} + 0,7 \cdot Q_{k,es}) = 1,35 \cdot G_k + 1,5 \cdot F_{k,w} + 0,75 \cdot Q_{k,n} + 1,05 \cdot Q_{k,es}$$

- Koeficijent "povoljnog" dejstva stalnog opterećenja: $\gamma_{Gj,inf}=1,0$

a. zategnuta spoljašnja ivica stuba

a.1 MINIMALNA sila pritiska

$$M_{Ed} = 1.35 \times 100 + 1.5 \times 200 = 435 \text{ kNm}$$

$$N_{Ed} = 0$$

$$\text{pretp. } d_1 = 7 \text{ cm} \Rightarrow d = 65 - 7 = 58 \text{ cm}$$

$$\text{C25/30} \Rightarrow f_{cd} = 14.2 \text{ MPa}$$

$b = 25$



$$k = \frac{58}{\sqrt{\frac{435 \times 10^2}{25 \times 1.42}}} = 1.657 \Rightarrow \varepsilon_{s1} < 2.5\%$$

Kako je $\varepsilon_{s1} < 2.5\%$, presek se **OBOSTRANO ARMIRA**.

usvojeno $\varepsilon_{s1,lim} = 2.5\%$ $\Rightarrow k_{lim} = 1.672$, $\omega_{Rd,lim} = 47.222\%$

$$M_{Rd,lim} = \left(\frac{58}{1.672} \right)^2 \times 25 \times 1.42 \times 10^{-2} = 427.2 \text{ kNm}$$

$$\Delta M = 435 - 427.2 = 7.8 \text{ kNm}$$

$$pretp.d_2 = 5 \text{ cm} \Rightarrow A_{s2} = \frac{7.8 \times 10^2}{(58 - 5) \times 43.5} = 0.34 \text{ cm}^2$$

$$\varepsilon_{s2} = \frac{\xi_{lim} - \frac{d_2}{d}}{\xi_{lim}} \varepsilon_{cu2} = \frac{0.584 - \frac{5}{58}}{0.584} \cdot 3.5 = 2.98 > 2.175 = \frac{435}{200} \left(= \frac{f_{yd}}{E_s} \right)$$

$$A_{s1} = 47.222 \times \frac{25 \times 58}{100} \times \frac{1.42}{43.5} + 0.34 = 22.69 \text{ cm}^2$$



a. zategnuta spoljašnja ivica stuba

a.2 MAKSIMALNA sila pritiska

a.2.1 dominantno promenljivo – VETAR

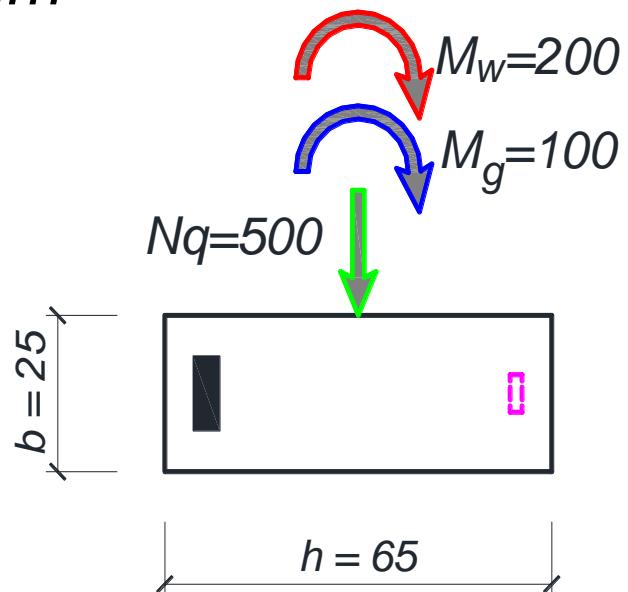
$$1,35 \cdot G_k + 1,5 \cdot (F_{k,w} + 0,5 \cdot Q_{k,n} + 0,7 \cdot Q_{k,es}) = 1,35 \cdot G_k + 1,5 \cdot F_{k,w} + 0,75 \cdot Q_{k,n} + 1,05 \cdot Q_{k,es}$$

$$M_{Ed} = 1.35 \times 100 + 1.5 \times 200 = 435 \text{ kNm}$$

$$N_{Ed} = 1.5 \times 0.7 \times 500 = 525 \text{ kN}$$

$$M_{Eds} = 435 + 525 \times \left(\frac{0.65}{2} - 0.07 \right) = 568.9 \text{ kNm}$$

$$k = \frac{58}{\sqrt{\frac{568.9 \times 10^2}{25 \times 1.42}}} = 1.449 \Rightarrow \varepsilon_{s1} < 2.5\%$$



Kako je $\varepsilon_{s1} < 2.5\%$, presek se OBOSTRANO ARMIRA.

usvojeno $\varepsilon_{s1,lim} = 2.5\%$ $\Rightarrow k_{lim} = 1.672$, $\omega_{Rd,lim} = 47.222\%$

$$M_{Rd,lim} = \left(\frac{58}{1.672} \right)^2 \times 25 \times 1.42 \times 10^{-2} = 427.2 \text{ kNm}$$

$$\Delta M = 568.9 - 427.2 = 141.7 \text{ kNm}$$

$$pretp.d_2 = 5 \text{ cm} \Rightarrow A_{s2} = \frac{141.7 \times 10^2}{(58 - 5) \times 43.5} = 6.15 \text{ cm}^2$$

$$\varepsilon_{s2} = \frac{\xi_{lim} - \frac{d_2}{d}}{\xi_{lim}} \varepsilon_{cu2} = \frac{0.584 - \frac{5}{58}}{0.584} \cdot 3.5 = 2.98 > 2.175 = \frac{435}{200} \left(= \frac{f_{yd}}{E_s} \right)$$

$$A_{s1} = 47.222 \times \frac{25 \times 58}{100} \times \frac{1.42}{43.5} - \frac{525}{43.5} + 6.15 = 16.4 \text{ cm}^2$$



a. zategnuta spoljašnja ivica stuba

a.2 MAKSIMALNA sila pritiska

a.2.2 dominantno promenljivo – KORISNO

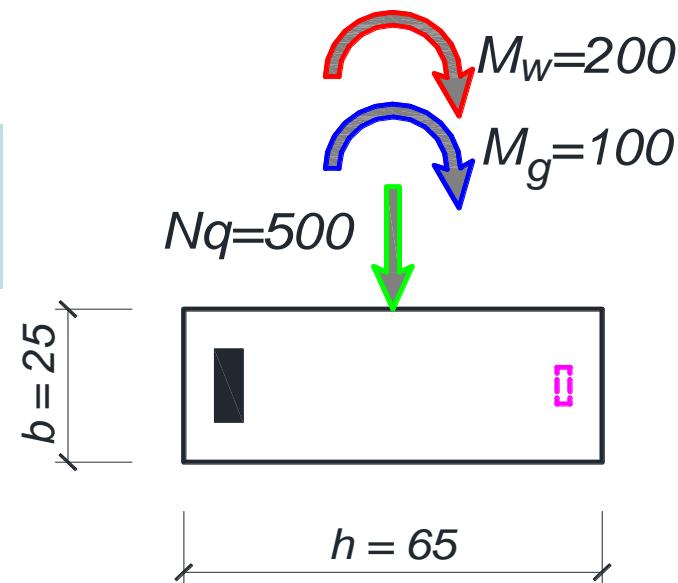
$$1,35 \cdot G_k + 1,5 \cdot (Q_{k,es} + 0,5 \cdot Q_{k,n} + 0,6 \cdot F_{k,w}) = 1,35 \cdot G_k + 1,5 \cdot Q_{k,es} + 0,75 \cdot Q_{k,n} + 0,9 \cdot F_{k,w}$$

$$M_{Ed} = 1.35 \times 100 + 1.5 \times 0.6 \times 200 = 315 \text{ kNm}$$

$$N_{Ed} = 1.5 \times 500 = 750 \text{ kN}$$

$$M_{Eds} = 315 + 750 \times \left(\frac{0.65}{2} - 0.07 \right) = 506.3 \text{ kNm}$$

$$k = \frac{58}{\sqrt{\frac{506.3 \times 10^2}{25 \times 1.42}}} = 1.536 \Rightarrow \varepsilon_{s1} < 2.5\%$$



Kako je $\varepsilon_{s1} < 2.5\%$, presek se OBOSTRANO ARMIRA.

usvojeno $\varepsilon_{s1,lim} = 2.5\%$ $\Rightarrow k_{lim} = 1.672$, $\omega_{Rd,lim} = 47.222\%$

$$M_{Rd,lim} = \left(\frac{58}{1.672} \right)^2 \times 25 \times 1.42 \times 10^{-2} = 427.2 \text{ kNm}$$

$$\Delta M = 506.3 - 427.2 = 79.1 \text{ kNm}$$

$$pretp.d_2 = 5 \text{ cm} \Rightarrow A_{s2} = \frac{79.1 \times 10^2}{(58 - 5) \times 43.5} = 3.43 \text{ cm}^2$$

$$\varepsilon_{s2} = \frac{\xi_{lim} - \frac{d_2}{d}}{\xi_{lim}} \varepsilon_{cu2} = \frac{0.584 - \frac{5}{58}}{0.584} \cdot 3.5 = 2.98 > 2.175 = \frac{435}{200} \left(= \frac{f_{yd}}{E_s} \right)$$

$$A_{s1} = 47.222 \times \frac{25 \times 58}{100} \times \frac{1.42}{43.5} - \frac{750}{43.5} + 3.43 = 8.54 \text{ cm}^2$$



Mmax, Nmin

$$A_{s1} = 22.69 \text{ cm}^2$$

$$A_{s2} = 0.34 \text{ cm}^2$$

Mmax, Nmax

Dominantan vetrar
Mmax

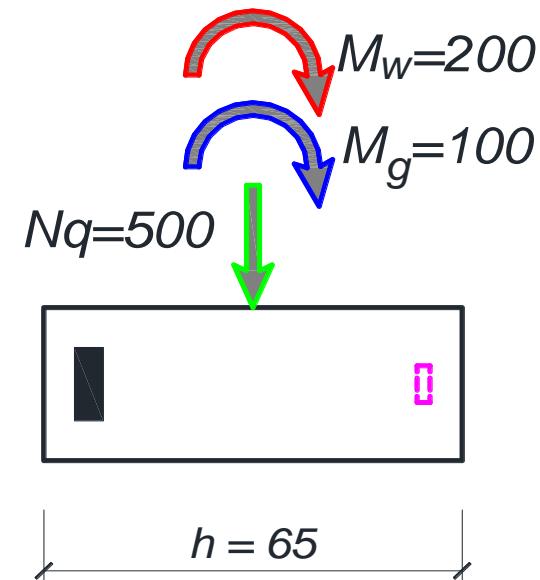
$$A_{s1} = 16.40 \text{ cm}^2$$

$$A_{s2} = 6.15 \text{ cm}^2$$

Dominantno korisno
Nmax

$$A_{s1} = 8.54 \text{ cm}^2$$

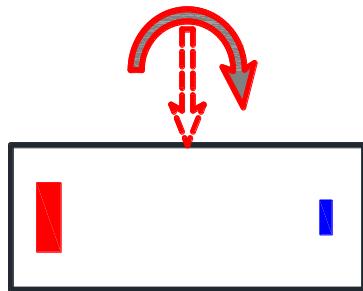
$$A_{s2} = 3.43 \text{ cm}^2$$



POTREBNO:

22.69

6.15



$$spolja: A_{s,potr.} = \max \left\{ \begin{array}{l} 22.69 \\ 16.40 \\ 8.54 \end{array} \right\} = 22.69 \text{ cm}^2$$

$$unutra: A_{s,potr.} = \max \left\{ \begin{array}{l} 0.34 \\ 6.15 \\ 3.43 \end{array} \right\} = 6.15 \text{ cm}^2$$

$$A_{s1,min} = \begin{cases} 0.26 \cdot \frac{2.6}{500} \cdot 25 \cdot 60 = 2.0 \text{ cm}^2 \\ 0.0013 \cdot 25 \cdot 60 = 1.95 \text{ cm}^2 \end{cases}$$
$$A_{s1,min} = 2.0 \text{ cm}^2$$

b. zategnuta unutrašnja ivica stuba

b.1 MINIMALNA sila pritiska

$$M_{Ed} = 1.0 \times (-100) + 1.5 \times 200 = 200 \text{ kNm}$$

$$N_{Ed} = 0$$

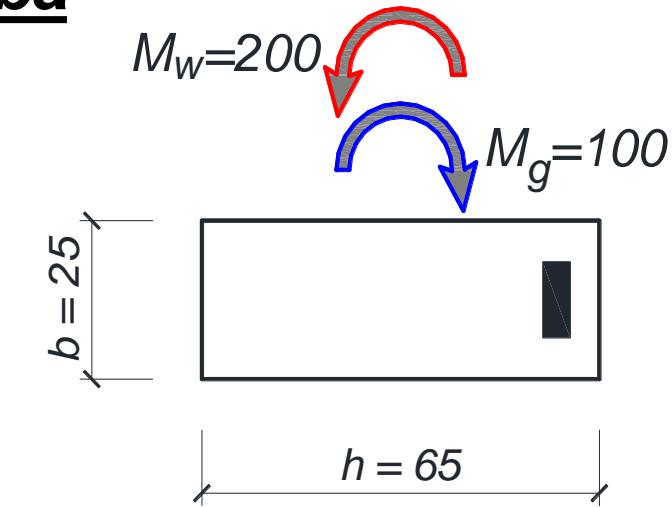
pretp. $d_1 = 5 \text{ cm} \Rightarrow d = 65 - 5 = 60 \text{ cm}$

$$\text{C25/30} \Rightarrow f_{cd} = 14.2 \text{ MPa}$$

$$k = \frac{60}{\sqrt{\frac{200 \times 10^2}{25 \times 1.42}}} = 2.528$$

$$\varepsilon_c / \varepsilon_{s1} = 3.5 / 13.18\% \Rightarrow \omega_1 = 16.982\%$$

$$A_{s1} = 16.982 \times \frac{25 \times 60}{100} \times \frac{1.42}{43.5} = 8.31 \text{ cm}^2$$



b. zategnuta unutrašnja ivica stuba

b.2 MAKSIMALNA sila pritiska

b.2.1 dominantno promenljivo – VETAR

$$1,35 \cdot G_k + 1,5 \cdot (F_{k,w} + 0,5 \cdot Q_{k,n} + 0,7 \cdot Q_{k,es}) = 1,35 \cdot G_k + 1,5 \cdot F_{k,w} + 0,75 \cdot Q_{k,n} + 1,05 \cdot Q_{k,es}$$

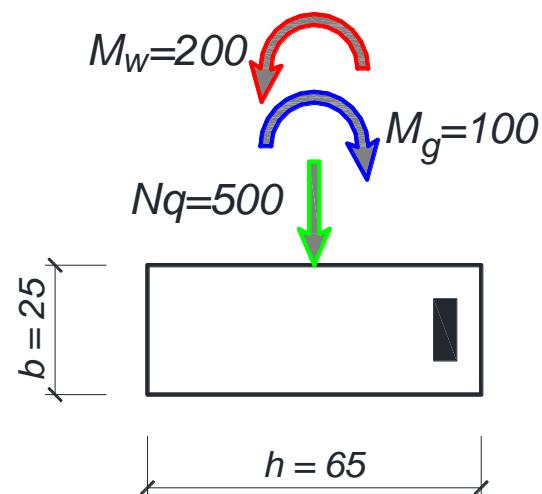
$$M_{Ed} = 1.0 \times (-100) + 1.5 \times 200 = 200 \text{ kNm}$$

$$N_{Ed} = 1.5 \times 0.7 \times 500 = 525 \text{ kN}$$

$$M_{Eds} = 200 + 525 \times \left(\frac{0.65}{2} - 0.05 \right) = 443.4 \text{ kNm}$$

$$k = \frac{60}{\sqrt{\frac{344.4 \times 10^2}{25 \times 1.42}}} = 1.926 \Rightarrow \frac{\varepsilon_c / \varepsilon_{s1}}{\omega} = 3.5 / 5.247\% \quad \omega = 32.391\%$$

$$A_{s1} = 32.391 \times \frac{25 \times 60}{100} \times \frac{1.42}{43.5} - \frac{525}{43.5} = 3.79 \text{ cm}^2$$



b. zategnuta unutrašnja ivica stuba

b.2 MAKSIMALNA sila pritiska

b.2.2 dominantno promenljivo – KORISNO

$$1,35 \cdot G_k + 1,5 \cdot (Q_{k,es} + 0,5 \cdot Q_{k,n} + 0,6 \cdot F_{k,w}) = 1,35 \cdot G_k + 1,5 \cdot Q_{k,es} + 0,75 \cdot Q_{k,n} + 0,9 \cdot F_{k,w}$$

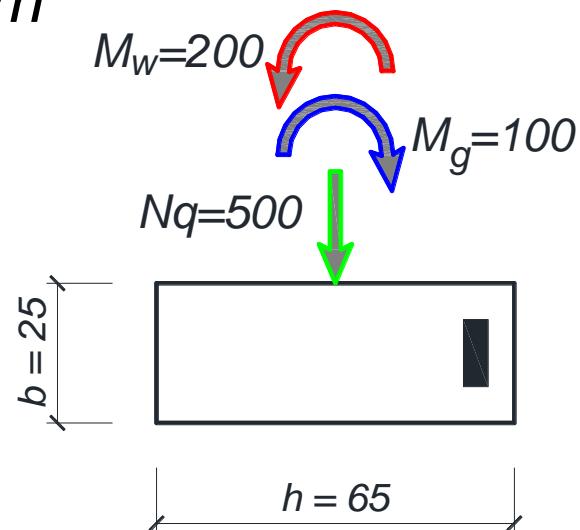
$$M_{Ed} = 1.0 \times (-100) + 1.5 \times 0.6 \times 200 = 80 \text{ kNm}$$

$$N_{Ed} = 1.5 \times 500 = 750 \text{ kN}$$

$$M_{Eds} = 80 + 750 \times \left(\frac{0.65}{2} - 0.05 \right) = 286.25 \text{ kNm}$$

$$k = \frac{60}{\sqrt{\frac{286.25 \times 10^2}{25 \times 1.42}}} = 2.113 \Rightarrow \frac{\varepsilon_c / \varepsilon_{s1}}{\omega} = 3.5 / 7.40\% \quad \omega = 25.994\%$$

$$A_{s1} = 25.994 \times \frac{25 \times 60}{100} \times \frac{1.42}{43.5} - \frac{750}{43.5} = -4.51 \text{ cm}^2$$



Mmax, Nmin

$$A_{s1} = 8.31 \text{ cm}^2$$

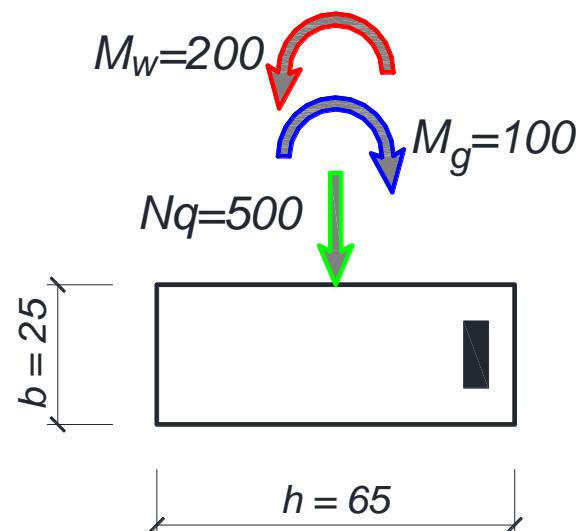
Mmax, Nmax

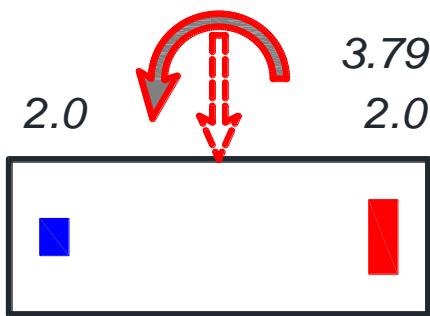
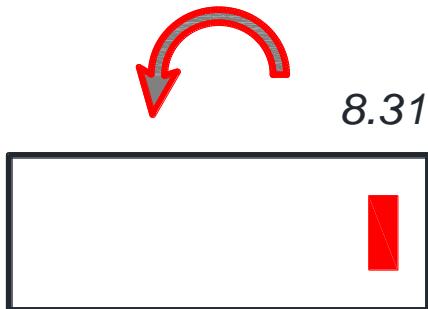
Dominantan vетар
Mmax

$$A_{s1} = 3.79 \text{ cm}^2$$

Dominantno korisno
Nmax

$$A_{s1} = -4.51 \text{ cm}^2$$





spolja: $A_{s,potr.} = \max \begin{Bmatrix} 0 \\ 2.0 \end{Bmatrix} = 2.0 \text{ cm}^2$

unutra: $A_{s,potr.} = \max \begin{Bmatrix} 8.31 \\ 3.79 \\ 2.0 \end{Bmatrix} = 8.31 \text{ cm}^2$

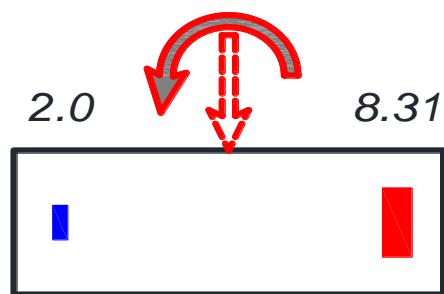
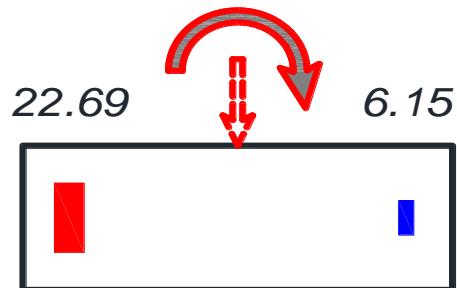
POTREBNO:

2.0 8.31



$$A_{s1,min} = \begin{cases} 0.26 \cdot \frac{2.6}{500} \cdot 25 \cdot 60 = 2.0 \text{ cm}^2 \\ 0.0013 \cdot 25 \cdot 60 = 1.95 \text{ cm}^2 \end{cases}$$

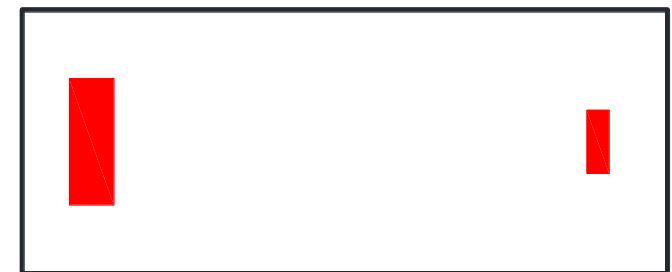
$A_{s1,min} = 2.0 \text{ cm}^2$



POTREBNO:

22.69

8.31



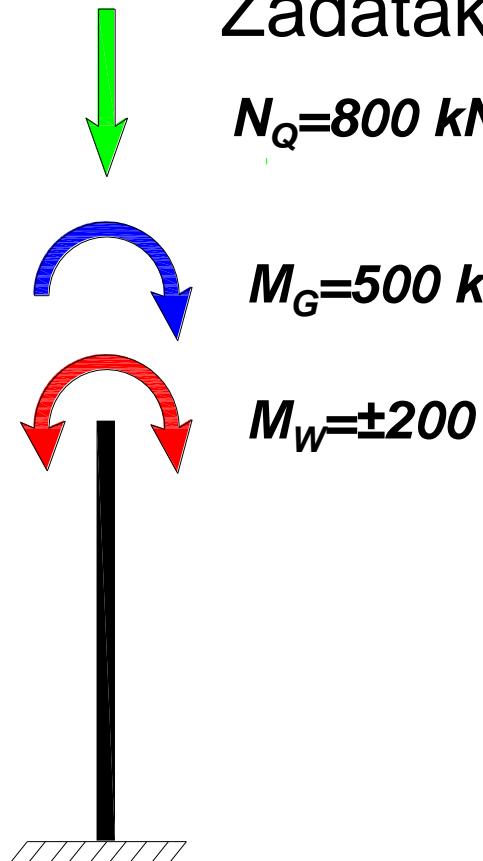
$$spolja: \quad A_{s,potr.} = \max \left\{ \frac{22.69}{2.0} \right\} = 22.69 \text{ cm}^2$$

5Ø25 (24.55 cm²)

$$unutra: \quad A_{s,potr.} = \max \left\{ \frac{6.15}{8.31} \right\} = 8.31 \text{ cm}^2$$

2Ø25 (9.82 cm²)

Zadatak 21 – KOMBINOVANJE OPTEREĆENJA



$$N_Q = 800 \text{ kN}$$

$$M_G = 500 \text{ kNm}$$

$$M_W = \pm 200 \text{ kNm}$$

$$\curvearrowright M_{Ed} = 1.35 * 100 + 1.5 * 200 = 435 \text{ kNm}$$

$$N_{Ed} = 0$$

$$\Rightarrow A_{s1} = 24.8 \text{ cm}^2 \quad A_{s2} = 0.3 \text{ cm}^2$$

$$\curvearrowright M_{Ed} = 1.35 * 100 + 1.5 * 200 = 435 \text{ kNm}$$

$$N_{Ed} = 1.5 * 0.7 * 800 = 840 \text{ kN}$$

$$\Rightarrow A_{s1} = 14.3 \text{ cm}^2 \quad A_{s2} = 9.14 \text{ cm}^2$$

$$\curvearrowright M_{Ed} = 1.35 * 100 + 1.5 * 0.6 * 200 = 435 \text{ kNm}$$

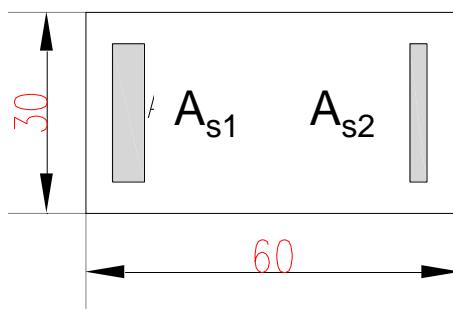
$$N_{Ed} = 1.5 * 800 = 1200 \text{ kN}$$

$$\Rightarrow A_{s1} = 4.7 \text{ cm}^2 \quad A_{s2} = 7.8 \text{ cm}^2$$

$$\curvearrowleft M_{Ed} = 1.0 * (-100) + 1.5 * 200 = 200 \text{ kNm}$$

$$N_{Ed} = 0$$

$$\Rightarrow A_{s2} = 9.77 \text{ cm}^2$$



Zadatak 21 – KOMBINOVANJE OPTEREĆENJA

Dimenzionisati stub prikazan na skici.

C30/37 B500 B
b/h=30/60 cm

